## Absorber Design and Performance in Vapour Absorption Refrigeration System : A Review

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**Abstract** - The absorber is a major component of Absorption cycle systems, and its performance directly impacts the overall size, performance, first-cost and energy supplies of these devices. In this paper a review of the main experimental, analytical results and review of different absorber designs reported in absorption refrigeration cycles is presented. It is shown that most of the experimental and analytical work found in the literature has focused on the particularly simplified case of absorption in falling film absorber and bubble mode absorber while there are only few papers on flat plate absorber or slug flow absorber. There are also work on comparison of absorber design for better performance. But there are lesser work available on the effect of heat transfer with increasing circulation rate or absorber temperature.

*Key Words*: Vapour absorption refrigeration system, Absorber design, etc.

#### **1. INTRODUCTION**

Ammonia–water absorption refrigeration system has drawn increasing attention in recent years. Absorption refrigeration system has much superiority in utilizing industrial waste heat and other low grade heat resources, which is beneficial to environmental protection and energy saving. However, the coefficient of performance (COP) of ammonia–water absorption refrigeration system is relatively low and the equipment is much bigger and heavier than vapour compression system with the same capacity. Many researchers have been conducted on improving the performance of ammonia–water absorption refrigeration.

Absorber is the key equipment in ammonia–water absorption refrigeration system. Absorption enhancement is an effective way to improve the performance of ammonia– water absorption refrigeration. The objective of this paper is to review the significant effort that have been made to develop mathematical, experimental model to analyse the effect of varied operating conditions on the outlet conditions.

# **1.1** Absorber in vapour absorption refrigeration cycle

Vapour absorption refrigeration cycles produce a cooling effect by removing heat and transferring this heat to a vaporized working fluid called "refrigerant". An absorption cooling system basically consists of an evaporator, an absorber, a generator, a condenser, an heat exchanger and requires two fluids: the refrigerant and an absorber solution. In the absorption cooling cycle the working fluid undergoes a phase change in the condenser and evaporator, and the absorbent solution, a change in concentration in the generator and the absorber.

The refrigerant flows into the evaporator, where it evaporates at a reduced pressure and temperature, taking heat from environment . The refrigerant vapour from the evaporator is absorbed at low pressure into the concentrated absorber solution in the absorber. A quantity of heat is released as much as the refrigerant vapour is absorbed. This heat is removed by some cooling fluid from the absorber. In the generator, a part of the working fluid is vaporized from the diluted absorber solution by addition of a quantity of heat at high temperature and pressure. The working fluid vapour is condensed at high pressure and temperature in the condenser with removal of heat to the ambient. The working fluid liquid in the condenser is returned to the evaporator through the expansion valve. Then the absorption cycle repeats from the evaporator. Figure 1.0 shows a schematic diagram of the described cycle.



Fig 1. Schematic diagram of vapour absorption refrigeration system

#### 2. Literature review

There are lots of work done in the absorber design and its effectiveness. In some papers they have design the absorber and noted down the effect of various inlet conditions on the outlet parameters. On analysis of these papers we have divided the papers in three section mainly : experimental,

Volume: 05 Issue: 05 | May-2018 IRIET

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e-ISSN: 2395-0056 p-ISSN: 2395-0072

temperatu

l analysis of

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theoretical and review papers. In case of experimental review we have included only those papers which has used some experimental set-up to derive a result. In case of theoretical review we have included those papers which has prove some findings through analytical ways using equations. In case of review paper it includes all the review work done on the absorber design and performance.

### 2.1 Experimental review

In case of falling film its seen that vapour absorption is increased by film inverting design and by establishing magnetic field in same direction as falling film [17,7]. Increase in solution flow rate increases absorber heat duty, overall heat transfer coefficient and solution heat transfer[9].

In flat plate heat transfer coefficient decreases with increase in Reynolds number and in case of flat sheet hydrophobic membrane should be as thin as possible and pore diameter should be in between  $0.3\mu m$  and  $0.1\mu m$ [15].

In counter current slug flow absorber the absorption length decreases with increasing the weak solution flow rate and with decreasing the gas flow rate and with increase of thermal heat transfer performance of the coolant side[4].

In bubble mode absorber the decrease in temperature and concentration leads to decrease in region of gas absorption. When ammonia vapour was injected flux were in the range of 0.0025-0.0063 kgm<sup>-2</sup>s<sup>-1</sup>, the solution heat transfer coefficient varied between 2.7 and 5.4 kW m<sup>-2</sup> K<sup>-1</sup>, the absorber thermal load from 0.5 to 1.3 kW[20]. Absorber heat load increases with circulation ratio and absorber temperature increase whereas decreases with generator temperature. Absorber heat transfer effectiveness increases with generator temperature increase whereas decreases with circulation ratio<sup>[27]</sup>. Absorption rate achieved with micro-finned tube is 1.7 times higher than the smooth tube and absorption mass flux increases when tube diameter is reduced and decreases when tube length is increased[1].

Table -1: Experimental work in Absorber of VAS

AUTHOR	DESCRIPTI	YEA	METHODOL	FINDINGS
/S	ON	R	OGY	
Raisul	Performanc	200	Experimenta	About
et.al [17]	e study of a	3	1	100%
	falling-film		investigation	increase
	absorber		of	in vapour
	with a film-		developmen	absorptio
	inverting		t of film-	n rate is
	configuratin		inverting	obtained.
			design for	
			falling-film	
			absorbers.	
Jae-Cheol	A study on	200	Numerical	With the
et.al [3]	numerical	3	and	decrease
	simulations		experimenta	in

	s for mass transfer in bubble mode absorber of ammonia and water		a bubble mode absorber.	concentra tion the region of gas absorptio n decreases. Absorptio n performa nce of the counter- current flow was superior to that of co- current.
Kim et.al [4]	Developme nt of a slug flow absorber working with ammonia- water mixture: part I—flow characteriza tion and experiment al investigatio n	200 3	Experimenta l investigation of counter- current slug flow absorber of ammonia- water for low solution flow rate.	The absorptio n length decreases with increasing the weak solution flow rate and with decreasin g the gas flow rate and with increase of thermal heat transfer performa nce of the coolant side
Kyongmi n K. and Siyoung J. [6]	Effect of vapor flow on the falling-film heat and mass transfer of the ammonia/w ater absorber	200 4	Effect of the vapour flow direction on the absorption heat and mass transfer has been investigated for a falling- film helical coil absorber for solution concentratio ns of (3. 14.	Heat and mass transfer is deteriorat ed in the counter- current flow. The effect of vapour flow direction decreased with increasing concentra tion of

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International Research Journal of Engineering and Technology (IRJET) e-ISS

e-ISSN: 2395-0056 p-ISSN: 2395-0072

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Jesus et.al [20]	Experiment al study of an ammonia- water bubble absorber using a plate heat exchanger for absorption refrigeratio n machines	200 9	and 30%). Experimenta l analysis in which ammonia vapour was injected in bubble mode into the solution.	ammonia solution. Flux were in the range of 0.0025– 0.0063 kgm <sup>-2</sup> s <sup>-1</sup> , the solution heat transfer coefficient varied between 2.7 and 5.4 kW m <sup>-2</sup> 2 K <sup>-1</sup> , the absorber thermal load from 0.5 to 1.3 kW. The	-	Lee et.al [9]	Measureme nt of absorption rates in horizontal- tube falling- film ammonia- water absorbers	201 2	solution. Experimenta l investigation of Heat and mass transfer in a horizontal- tube falling- film ammonia- water absorber.	in concentra tion of R134a. The absorber heat duty, the overall heat transfer coefficient , and the solution heat transfer coefficient were found to increase with increasing solution flow rate.
[7]	al study on ammonia- water falling film absorption in external magnetic fields	0	l analysis to investigate the effect of magnetic fields of different intensities and different directions.	magnetic field with the same direction as falling film enhances the absorptio n, and the magnetic field with the direction against falling film weakens the absorptio n.		Cesar et.al [12]	Heat and mass transfer in a bubble plate absorber with NH3/LiNO3 and NH3/(LiNO 3 + H2O) mixtures	201 3	Experimenta l test for the absorber characteriza tion at different operation conditions.	For both binary and ternary mixtures, the mass absorptio n flux, heat transfer coefficient , sub- cooling and mass transfer coefficient increase as the solution flow rate increases.
Harikrish nan et.al [22]	Investigatio ns on heat and mass transfer characterist ics of falling film horizontal tubular absorber	201 1	Experimenta l investigation of heat and mass transfer characteristi cs of absorber for refrigerant, R134a absorbed by R134a- DMAC	Heat and mass transfer coefficient s increases by higher solution flow rate decrease in the generator heat input increase		Suresh M. and Mani A. [27]	Heat and mass transfer studies on a compact bubble absorber in R134a-DMF solution based vapour absorption refrigeratio n system	201 3	Experimenta l investigation s of heat and mass transfer characteristi cs of Tetrafluoro ethane (R134a) in Dimethyl formamide	Absorber heat load increases with circulatio n ratio and absorber temperatu re increase whereas decreases with



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p-ISSN: 2395-0072

			(DMF) solution in a compact bubble absorber.	generator temperatu re. Absorber heat transfer effectiven ess increases with				drops occurring inside a tube-in-tube refrigerant cooled absorber (RCA).	has been found for the calculatio n of pressure drop in the annulus.
Carlos A.	Effect of	201	Experimenta	generator temperatu re increase whereas decreases with circulatio n ratio. Results	Domingu ez- Inzunza et.al [14]	Experiment al assessment of an absorption cooling system utilizing a falling film absorber	6	A parametric study of coefficients of performance and cooling capacities at different operating conditions.	It was seen that the coefficient s of performa nce increased with the increase
Mahmou d B and Manel V [1]	advanced surfaces on the ammonia absorption process with NH3/LiNO3 in a tubular bubble absorber	4	l investigation s are done to analyze the effect of surface enhancemen t using smooth tube and an internally micro-finned tube.	show that the absorptio n rate achieved with the micro- finned tube is up to 1.7 times higher than with the smooth tube and absorptio		and generator			of the generator temperatu re and decreased with the increase in the temperatu re of the cooling water supplied to the condenser and absorber.
				n mass flux increases when tube diameter is reduced and decreases when tube length is increased.	Delphine et.al [16]	Modeling and experiment al study of an ammonia- water falling film absorber	201 6	A numerical and experimenta l study to analyse the heat and mass transfers that take place in a plate heat exchanger used as	The compariso n between experime ntal and numerical results in terms of temperatu re, mass flow rate and concentra
Tommaso et.al [13]	Modelling and experiment al validation of a tube-in- tube refrigerant cooled	201 5	Experimenta l investigation s for predicting heat and mass transfer and	Higher the load at the RCA, the better the model accuracy. A deviation				absorber.	tion in the liquid solution at the outlet of the absorber shows a
	absorber		pressure	of 0-20%					maximal



International Research Journal of Engineering and Technology (IRJET) e-ISSN: 2

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				relative
				error of 1
				% is
				observed.
Delphine et. al [2]	Experiment al and numerical study of a falling film absorber in an ammonia- water absorption chiller	201 7	An experimenta l and numerical study of heat and mass transfer in a falling film absorber is determined.	The model is validated with experime ntal data and a maximal relative error of 15% is observed between experime ntal and
				roculte
Devidence	The second second	201	٨	Tesuits.
Berdasco	ineoretical	201	A hudronhohio	ine model the
IVI, Coronac	allu	/	nyurophobic	hudropho
Coronas	experiment		micro-	hydropho
A. and	al study of		porous	DIC
Valles M.	the		membrane	membran
[15]	ammonia/w		contactor	e should
	ater		was	be as thin
	absorption		proposed	as
	process		and studied	possible
	using a flat		experimenta	and the
	sneet		lly and	pore
	membrane		analytically	diameter
	module		as an	Detween
			absorber for	0.03μm
			an . ,	and
			ammonia/w	0.10μm.
			ater	
			absorption	
			cycle.	

#### 2.2 Theoretical review

For packed bed absorber a bed height less than 0.7 m guarantees absorption efficiency better than 91%[11]. Local absorption rate of the bubble mode was always higher than that of the falling film and Bubble absorption is more efficient for low solution flow rates[18,19]. In slug flow absorber the heat and mass transfer coefficient at the frost flow region is higher than that at the slug flow region [5]. In vertical tubular absorbers absorption process progresses rapidly in the churn and in the slug flow regions but slows down in the bubbly flow and absorption process occurs slowly from the first to the last tube row[21,28]. In counter-current vapour flow absorber interface temperature is always greater than the bulk liquid temperature and absorption rate increases as the coolant inlet and solution inlet temperatures decrease, and as the coolant flow rate increases[29]. In bubble absorber the reduction in coolant inlet temperature significantly enhances

the mass transfer rates [8,25]. In falling film the absorber heat duty, the overall heat transfer coefficient, and the solution heat transfer coefficient were found to increase with increasing solution flow rate and that the influence of released differential heat of solution within the bulk is relatively small [25,26]. For a membrane-based absorber the porosity and pore diameter of the membrane and the solution channel width should be maximum and solution channels depth, the thicknesses of the membrane and of the wall separating the solution and the cooling water and also the cooling water channels depth should be minimum [30].

Table -2:	Theoretical	work in	Absorber	of VAS
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AUTHO	DESCRIPTI	YEA	METHODOL	FINDINGS
R/S	ON	R	OGY	
Selim A. M and Elsayed M. M [11]	Performanc e of a packed bed absorber for aqua ammonia absorption refrigeratio n system	199 9	A mathematica l model is used to predict the performance of the bed at various design and operating conditions.	The results shows that changing the bed pressure and/or the vapour inlet temperatu re have negligible effect on the performa nce of the bed. A bed height less than 0.7 m guarantee s absorptio n efficiency better than 91%.
Yong et. al [18]	Analytical investigatio n of two different absorption modes: falling film and bubble types	200 0	Parametric analysis is used to evaluate the effects of heat and mass transfer areas on the absorption rate for falling film and bubble modes.	Local absorptio n rate of the bubble mode was always higher than that of the falling film model leading to

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www.irjet.net

p-ISSN: 2395-0072

Kim et.al [5]	Developmen t of a slug flow absorber working with ammonia- water mitturo:	200 3	The study deals with a data reduction model for clarifying experimental results of a countor	about 48.7% smaller size of the heat exchanger The heat and mass transfer coefficient at the frost flow region is higher than that		Analysis of	200	A datailad	absorptio n rate increases as the coolant inlet and solution inlet temperatu res decrease, and as the coolant flow rate increases.
	part II— data reduction model for local heat and mass transfer characteriza tion		current slug flow absorber for significantly low solution flow rate.	at the slug flow region.	[28]	an air cooled ammonia- water vertical tubular absorber	7	analysis of an ammonia– water vertical tubular absorber cooled by air.	results show that the absorptio n process occurs slowly from the first to the
Jose et.al [21]	Ammonia– water absorption in vertical tubular absorbers	200 5	A detailed analysis of the heat and mass transfer processes in a co-current vertical tubular absorber.	The absorptio n process progresse s rapidly in the churn and in the slug flow regions but slows down in the bubbly					last tube row according to the air flow direction and the length of the tubes increases from the first row to the last one.
Nitin G and Yogi G [29]	Analysis of a counter- current vapor flow absorber	200 5	A analytical investigation of a combined heat and mass transfer process in a counter- current ammonia- water based absorber.	flow. The interface temperatu re is always greater than the bulk liquid temperatu re. In addition, the liquid-	Castro et.al [19]	Comparison of the performanc e of falling film and bubble absorbers for air- cooled absorption systems	200 9	A parametric study has been done on two air- cooled absorber falling film flow and bubble flow models are validated with experimental data.	Bubble absorptio n is more efficient for low solution flow rates.
				side heat transfer resistance is negligible and	Ruander C and Vinod N [8]	Heat and mass transfer characteristi cs of a constrained	201 1	A study of absorption of ammonia vapour bubbles into a	Results indicate that the reduction in coolant inlet

ISO 9001:2008 Certified Journal



International Research Journal of Engineering and Technology (IRJET) e-ISSN: 2395-0056

p-ISSN: 2395-0072

**TRJET** Volume: 05 Issue: 05 | May-2018

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	thin-film ammonia- water bubble absorber		constrained thin-film of ammonia- water solution is presented.	temperatu re significant ly enhances the mass transfer rates in both absorber geometrie s.		the performanc e of a membrane- based absorber		absorber using a micro- porous membrane as contactor between the vapour and the solution is done.	membran e and the solution channel width should be maximum and solution channels depth, the thickness
Sangso et.al [25]	Measureme nt of absorption rates in horizontal- tube falling- film ammonia- water absorbers	201 2	Heat and mass transfer in a horizontal- tube falling- film ammonia- water absorber was investigated.	The absorber heat duty, the overall heat transfer coefficient , and the solution heat transfer coefficient were found to increase with increasing solution	Mehdi et.al [10]	A detailed study on	201 7	A numerical model of a	es of the membran e and of the wall separatin g the solution and the cooling water and also the cooling water channels depth should be minimum. Results shows the
Mitterma ier et.al [26]	A numerical model for combined heat and mass transfer in a laminar liquid falling film with simplified hydrodyna mics	201 4	A numerical analysis describing heat and mass transfer of an absorbing or desorbing laminar liquid film flowing over a vertical isothermal plate.	flow rate. It is found that the influence of released differentia l heat of solution within the bulk is relatively small and mass transfer rate during absorptio n is higher than during desorptio	2.3 Rev	simultaneou s heat and mass transfer in an in-tube vertical falling film absorber		vertical in- tube falling film absorption heat exchanger utilizing NH3–H2O is developed.	main resistance s for heat and mass transfer are ones between gas and interface and majority of the gas gets absorbed by the film in the top segments of the pipes.
Venegas et.al [30]	Parametric study of operating and design variables on	201 6	A simulation of plate-and- frame micro- channel H2O-LiBr	n. The porosity and pore diameter of the	Maxin absorptio problem machine efficient	mum work on on in laminar ver , Adiabatic abso s whereas Bul [24,31]. The corr	availa tical fil rber re oble t elation	ble on simplifi lm which has the educes the size ype absorbers s for LiBr-H <sub>2</sub> O a	ed case of ewettability and cost of are more nd NH <sub>3</sub> -H <sub>2</sub> O

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www.irjet.net

e-ISSN: 2395-0056 p-ISSN: 2395-0072

Absorption Refrigeration in falling film and heat and mass transfer enhances as the Reynolds number is increased. And in lithium-bromide there were divergences between theoretical studies[32].

Table -3: Review work in Absorber of VAS

AUTHOR	DESCRIPTI	YEA	METHODOL	FINDING
/S	ON	R	OGY	S
Jesse D.	A critical	200	It reviews the	Most
K. and	review of	1	significant	work
Srinivas	models of		efforts that	found is
G. [24]	coupled		researchers	on the
	heat and		have made to	simplifie
	mass		mathematical	d case of
	transfer in		ly model the	absorptio
	falling-film		coupled neat	n in
	absorption		transfor	lainnai
			nhonomona	films of
			that occurs	minis of
			during falling	lithium
			film	bromide
			absorption	Sionnuc.
Ionathan	Performanc	201	It provides a	Falling
I and	e of	4	review of the	film
Rosenber	Different	-	literature on	absorber
g J. R [31]	Experiment		absorber	s has
0, 1,	al Absorber		design and its	wettabilit
	Designs in		performance	у
	Absorption		in absorption	problem.
	Heat Pump		cycles.	Adiabatic
	Cycle			absorber
	Technologi			reduces
	es: A			the size
	Review			and cost
				of
				machines
				. Bubble
				type
				absorber
				s are
				officient
Roothour	A Critical	201	It ravious the	In
n et al	Review of	201	heat and	ammonia
[32]	Heat and	<sup>′</sup>	mass transfer	-water
[32]	Mass		correlations	absorntio
	Transfer		in the falling	n
	Correlation		film absorber	processe
	s for LiBr-		technology.in	s. the
	$H_2O$ and		ammonia-	heat and
	NH <sub>3</sub> -H <sub>2</sub> O		water and	mass
	Absorption		lithium	transfer
	Refrigeratio		bromide-	enhances
	n Machines		water.	as the
	Using			Reynolds
	Falling			number
	Liquid Film			is

Technology	increased
	And in
	lithium-
	bromide
	there
	were
	divergen
	ces
	between
	theoretic
	al
	studies.

#### **3. CONCLUSIONS**

The absorber is the most important component of absorption machines, in general, its performance impacts directly in the size and energy supply of all absorption devices. There are lots of work done in the field of effect of absorber design on heat and mass transfer and there are ways to increase the heat and mass transfer by adopting certain design and inlet flow conditions. There are also work on comparison of absorber design for better performance. But there are lesser work available on the effect of heat transfer with increasing circulation rate or absorber temperature.

#### Experimental review

We have included papers from 2003-2017. There have been a literature gap of 5 years in between where mainly theoretical work was carried out. Majority of works were done on falling film absorber and bubble mode absorber while there are only few papers on flat plate absorber or slug flow absorber. Falling film absorber is the most common absorber but it has a wettability problem and bubble mode absorber provides better heat and mass transfer coefficient and thus making it more efficient.

#### Theoretical review •

We have considered papers from 1999-2017. There is no any significant literature gap which means the work is continuously being carry on. In this field significant work are carried on each absorber to increase its efficiency and performance. Numbers of work are carried on to visualise the effect of different design parameter on heat and mass transfer. But they do not show the effect of varying mass flow rate on the heat and mass transfer.

**Review** papers

There have been hardly few literature review on the design and performance of absorber. we have only 3 which are published in 2001, 2014 and 2017 in which two are on heat and mass transfer coefficient in falling film absorber and one is on performance of different absorber designs. It means that this is the regions were significant work is required to make the further investigation area to be defined.

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#### ACKNOWLEDGEMENT

The authors can acknowledge any person/authorities in this section. This is not mandatory.

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