

# Experimental Study on Flexural and Compressive behavior of Cold Formed Steel Back To Back Supacee Section

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**Abstract** - Cold formed steel sections or light gauge steel sections are thin walled sections which are gaining popularity in recent years. These sections are cold-formed from carbon or low alloy steel sheet, strip, plate, or flat bar in cold-rolling machines or by press considered and worked on as a replacement hot rolled section. Unusual sectional configurations can be produced economically by cold forming operations, and consequently favourable strength-to-weight ratios can be obtained. Supacee section is the special case c section. This section is equipped with both intermediate and edge stiffeners. This section is tested of its flexural and compressive behaviour (i.e., as both beam and column). In this present study the failure pattern and region of failure are to be analyzed.

**Key Words:** Cold Formed Steel, Supacee section, Flexural member, Compression member, Intermediate stiffener, Edge stiffener, Numerical analysis, Experimental analysis.

## 1. INTRODUCTION

Cold-formed steel (CFS) is the common term for products made by rolling or pressing steel into semi-finished or finished goods at relatively low temperatures (cold working). Cold-formed steel goods are created by the working of steel billet, bar, or sheet using stamping, rolling (including roll forming), or presses to deform it into a usable product. Cold-worked steel products, such as cold-rolled steel (CRS) bar stock and sheet, are commonly used in all areas of manufacturing of durable goods, such as appliances or automobiles, but the phrase cold-formed steel is most prevalently used to describe construction materials. In building construction, cold-formed steel products can be classified into three categories: members, panels, and prefabricated assemblies. Typical cold-formed steel members such as studs, track, purlins, girts and angles are mainly used for carrying loads while panels and decks constitute useful surfaces such as floors, roofs and walls, in addition to resisting in-plane and out-of-plane surface loads. Prefabricated cold-formed steel assemblies include roof trusses, panelized walls or floors, and other prefabricated structural assemblies. Supacee section has a strengthened cross section than traditional c section. It is equipped with four intermediate stiffeners in web region (V-shaped) and distinctive edge stiffener with a return lip, where the lip portion is bent additionally than conventional 90 degree bending from flanges towards the section. This section is to

analytically (ABAQUS software) and experimentally studied. The results of the both are compared with each other.

## 2. SECTION PROPERTIES (Supacee Section)

In cold-formed steel constructions, built-up beams and columns are often fabricated from two channel sections. Connecting two channels together is a technique which can achieve a structurally desirable cold-formed steel section. With this technique the structural strength capacity of the section is expected to be more than double. Traditional, field fabricated, back to back or I-beam headers, consisting of two "C" sections with the webs screwed back to back, are the most popular built-up configuration in the construction industry. Due to this higher strength 'Supacee sections' has been selected.

### 2.1 Specimen Details

The cross section of supacee section is shown in figure 1,

- Depth of web : 195mm
- Width of flange : 150mm
- Thickness : 2.5mm
- Corrugation depth : 10mm
- Lip of section : 25mm
- Return lip : 25mm

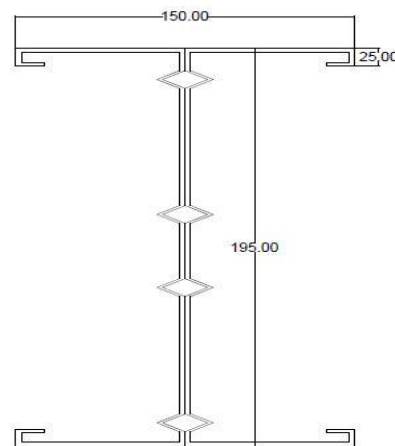


Fig -1: Cross Section of Supacee Section

## 2.2 Need of Supacee Section

- Supacee section is equipped both edge and web stiffener.
- This section has a distinct Edge stiffener. It has a return lip feature with a distinct extra projection than conventional 90 degree lip projection.
- Stiffener presented at web section is at distinct lengths, which are fixed after several experimental investigations.
- This distinctive web cross section (with 4 stiffeners) helps in effectively resisting the local buckling in web region.
- Return lip provision present helps in increasing load bearing capacity of the section and reducing the local buckling failure in flange region.

## 3. ABAQUS SOFTWARE

ABAQUS, It is a software application used for modeling, assembling, analysing and visualizing the finite element analysis result. ABAQUS is a software suite for finite element analysis and computer-aided engineering. ABAQUS provides the most complete and flexible solution to understand the detailed behaviour of a complex assembly, refine concepts for a new design, understand the behaviour of new materials, or simulate a discrete manufacturing process. ABAQUS 6.12 version software is used to create modelling, predict load, displacement, rotation, flexure behaviour for any kind of model.

Every complete finite-element analysis consists of 3 separate stages:

- Pre-processing or modelling: This stage involves creating an input file which contains an engineer's design for a finite-element analyzer (also called "solver").
- Processing or finite element analysis: This stage produces an output visual file.
- Post-processing or generating report, image, animation, etc. from the output file: This stage is a visual rendering stage

### 3.1 Software Analysis

The geometry of any section to be analysed are first modelled under various stages before analysing. This modelling is done to provide necessary details shape of model, dimensions of cross section, their interaction conditions, type of mesh used for meshing, the value of load applied and at which precise location. The column and beam specimen were modelled using a 3D modelling tool. Various iterations have to be given to the beam and column models to achieve its maximum load carrying capacity and its nature of failure at that load.

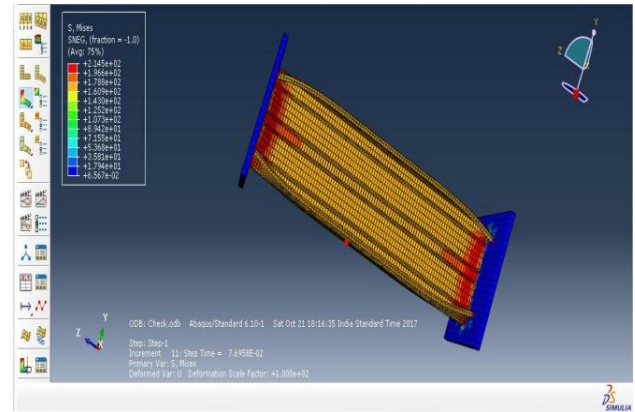


Fig -2: Failure pattern of column

The figure 2 indicate failure pattern of specimen when it is axially loaded from top (column). The area of failure is mainly in flange region. Due the provision of four intermediate stiffeners in web region there is very little damage even after reaching failure condition of the specimen. The maximum deflection value from ABAQUS software is 0.12 mm and ultimate load is 128.5kN. Global buckling occurs along the length of stiffened web section. The deflection increases till the middle section and decreases to the edge portion.

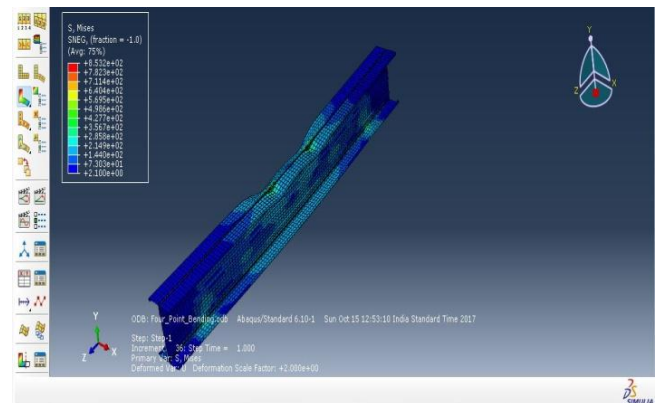


Fig -3: Failure pattern of beam

The figure 3 indicate failure pattern of supacee section on flexural loading condition. Here the area of failure is observed mainly around the area of loading and near support. The cause of failure noted is mainly due to local buckling. This local buckling in flange region leads to collapse of specimen and fail when reaching its maximum load. The maximum deflection value from ABAQUS software is 7.43 mm and ultimate load is 63kN.

## 4. EXPEIMENTAL ANALYSIS

The specimens are fabricated by locally available cold formed sheets. Four specimens were taken for testing (two specimens as a beam member and two specimens as a column member). The CFS sheet of 2.5mm is used for this supacee section. The specimen is kept back to back to make it as a "I" section or a built up back to back supacee "I" section. For beam specimens an additional 150x1200 mm plate is

provided only on top of the beam member over the flange at the point of loading. This is done to ensure the load is spread evenly to both flanges of the back to back built up supacee "I" section. Likewise 150\*200 mm plates are provided at top and bottom of the supacee column specimen. The supacee channels are connected back to back by 0.5 mm fillet welds at placed equal intervals. The yield strength of the cold formed steel sheets used is 350 N/mm<sup>2</sup>.

**4.1 Flexure Test Set-Up**

Flexural test evaluates the tensile strength of specimen indirectly. It tests the ability of steel beam to withstand failure in bending. The flexural test on beam can be conducted using either two point load test or centre point load test. The testing was carried out in a loading frame of 1000kN capacity. The specimens were tested for flexural strength under two-point loading. In two-point loading test loads were applied at one-third distance from the supports at a uniform rate till the ultimate failure of the specimens occurred. Beam deflections were measured at the centre of the beam using LVDT. The experimental setup is shown in figure 4. Deflection and failure pattern of the beam specimen for flexure test are shown in fig 4.



Fig -4: Experimental test setup for flexure test



Fig -5: Failure pattern of beam

Fig 5 shows the failure pattern of supacee beam. Supacee beam on loading in four point loading condition, experiences deflection. Failure of section is present in the flange region along the area of supports. Nature of buckling experienced is local buckling in flange region.

**4.2 Compressive Test Set-Up**

Axial loading test evaluates the compressive strength of specimen. It tests the ability of steel column to withstand when loaded in its centroidal axis. Unlike service load conditions, the behaviour of the axially compressed column is fully predictable under ultimate load conditions. As axial loading is increased, axial shortening of the column increases linearly up to about 80% of the ultimate load. The testing was carried out in a loading frame of 1000kN capacity. The specimens were tested for compressive strength. Load was to be applied from one end using a hydraulic jack while the other end is restrained against the frame setup. Here load is applied from the bottom and the restrained condition is met by resting the other end to the loading frame. Load is applied at a steady rate until failure and axial shortening of column were measured using LVDT. The experimental setup is shown in figure 4. Axial deformation of supacee column and its failure pattern are shown in fig 6.



Fig -6: Experimental test setup for compression test

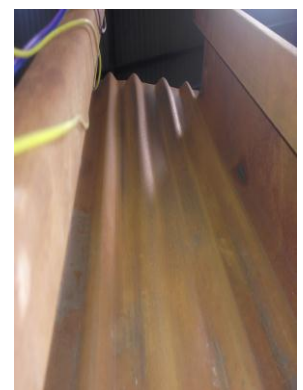


Fig -7: Failure pattern of column

Fig 7 shows the failure pattern of supacee column. Supacee column on loading in axial loading condition, experiences axial shortening. Failure of section is present in the web region along the point of loading. Nature of buckling experienced is distortional buckling in web region and flange at the end of section.

## 5. RESULTS AND DISCUSSIONS

### 5.1 Load vs Deflection Curve

Load bearing nature is the ability of a specimen to withstand without failing. This characteristic of a member is very important as this value is the base in designing of a structure.

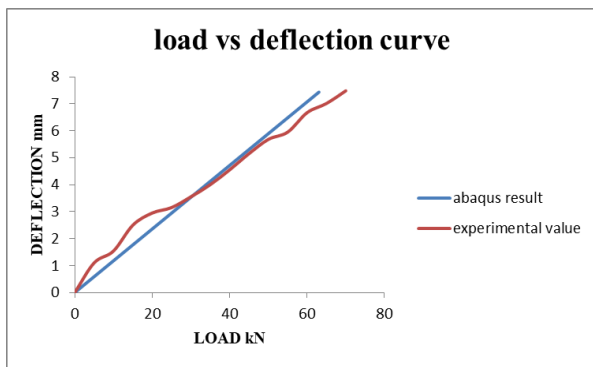


Chart -1: load vs deflection curve for supacee beam

Load with their corresponding deflection curve is depicted with values obtained from Abaqus software and experimental analysis are shown in chart 1. By experimental result the specimen yield's at 45 kN with a deflection of 5.15mm and fails at load of 70 kN at a deflection of 7.48 mm. By analytical result the specimen yield's at 43 kN with a deflection of 5.08mm and fails at load of 63 kN at a deflection of 7.44 mm.

### 5.2 Load vs Axial Deformation Curve

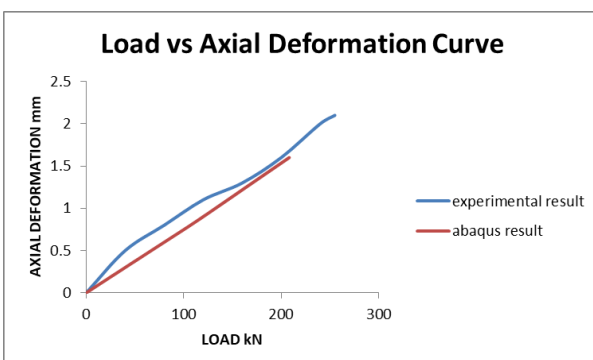


Chart -2: load vs axial deformation curve for supacee beam

Load with their corresponding axial deformation curve is depicted with values obtained from abaqus software and experimental analysis are shown in chart 2. By experimental

result the specimen yield's at 200 kN with a deflection of 1.4 mm and fails at load of 255 kN at a deflection of 2.1 mm. By analytical result the specimen yield's at 162 kN with a deflection of 1.2 mm and fails at load of 208 kN at a deflection of 1.6 mm.

## 6. CONCLUSION

- Supacee section as a flexural member, on analysis bears a maximum load of 70 kN where as conventional cold formed steel I section bears a load within the range of 28 kN to 35 kN for 1.2 meter span.
- Supacee section as a compressive member, on analysis bears a maximum load of 255 kN whereas conventional cold formed steel I section bears a load within the range 78 kN to 86 kN for a span of one meter.
- Numerical analysis using abaqus software is done to compare the results with experimental analysis. From the comparison we can see that the error percentage is less than 20 percent.
- This clearly indicates that this supacee section shows enhanced strength when compared to conventional built up I section for both compression and flexural member.
- This improved cross section enables the use of this section even as a primary compression member (as a column which cold formed steel section are not used till date) and as purlins and rafters in industrial roofing constructions.

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