# DEVELOPING OF AN EQUIVALENT RECTANUGLAR COLUMN FOR AN L-SHAPED RC COLUMN HAVING SIMILAR ULTIMATE LOAD MOMENT CHARACTERISTICS 

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#### Abstract

The structural characteristics of rectangular and circular columns can be easily analysed because the axis of centre of gravity lies within the section of the columns, whereas the centroidal axis lies outside the section in case of $L$ shaped columns. Due to this, the section characteristics of $L$ sections vary when compared to the other type of normal sections i.e.; rectangular and circular columns. Therefore this work deals with the study and analysis of strength parameters and nature of $L$ section with respect to the rectangular column. This is a work on L column, as there is a lack of adequate codal provisions of this type of columns. In this project the behaviour of L shaped Columns are interpreted in the form of Interaction Diagrams. In this work an attempt is made to obtain interaction curve for symmetrical L-shaped column and compare with that of equivalent rectangular column of different $B / D$ ratio.


Key Words: Xu , Pu, Mu, NA, Interaction curve.

## 1. INTRODUCTION

Columns are important elements which support the structures. They are the compression members and their failure may cause damage to the whole building. A column located in the building corner. In recent days irregular shaped columns are providing at the building corners and at enclosure of elevator shafts. The column may be of the shapes rectangular, circular, square, L shaped, T (tee) shaped etc. The size and cross section of the column depends on structure, height of the building and the loads acting on the structural member. The main aim of providing column is to resist against axial compression(P) and bending moments $\left(M_{x} M_{y}\right)$.These load and moment develop due to external loads, such as dead load, live load, and lateral forces resulting from wind load and seismic action and by unbalanced moments at connecting beams, vertical misalignments. IS code (IS 456-2000) and design aid (SP-16) follows the strength criteria as a support for designing reinforced concrete columns wherein the failure is defined when it comes to a limiting strain and stress in concrete and the reinforcement. An interaction diagram may be plot for any column including given specifications such as grade, percentage of steel, reinforcement detailing pattern,
dimension and shape of column by evaluating strain at various locations within the column considered, there by evaluating stress that return provides load and moment values, such numerous values of ultimate load and moment resisting capacity could be evaluated at different locations once the set of ultimate load and moment resistance values are obtained it could be graphically represented as an interaction diagram where load moment envelop serves as a failure curve implying that any combination of load and moment that falls within the envelop is safe and the loadmoment combination that falls on the curve as the maximum load-moment resisting capacity of the section. Therefore interaction diagrams are one of the importance factor in design of columns.

## 2. INTERACTION DIAGRAM

Interaction diagram shown in fig- 1 is a graph illustrating the capacity of a structural concrete member to resist a range of combinations of moment and axial force. The interaction diagram of the columns is drawn with a view to determine if the maximum axial load and moment exceeds the strength of the column. By changing the location of the neutral axis, giving different size of compressive and tension zones, each case will lead to a different capacity calculated from the strain distribution. Each point on the curve show design strength values of $P_{u}$ and $M_{u}$ linked to a specific eccentricity of loading wherein;
$P_{u}$ : ultimate load carrying capacity of concrete.
$\mathrm{M}_{\mathrm{u}}$ : ultimate moment carrying capacity of concrete.


Fig-1: Interaction curve

### 2.1 Salient points on the interaction curve

The salient points marked 1 to 5 in the interaction curve in fig-2 corresponds to the failure strain profiles.

- The point 1 in fig- 2 corresponds to the axial loading condition ith $\mathrm{e}=0$. In this case of pure axial compression, $\mathrm{M}_{\mathrm{uR}}=0$ and $\mathrm{P}_{\mathrm{uR}}$ is indicated as $\mathrm{P}_{\mathrm{u} 0}$ given by the equation $\mathrm{P}_{\mathrm{u} 0}=0.446 \mathrm{f}_{\mathrm{ck}} \mathrm{A}_{\mathrm{c}}+\mathrm{X} \mathrm{f}_{\mathrm{y}} \mathrm{A}_{\mathrm{s}}$

Where $\mathrm{A}_{\mathrm{c}}=$ Area of concrete excluding area of steel incorporated in the section
$\mathrm{A}_{\mathrm{s}}=$ Area of steel present in the section
$\mathrm{f}_{\mathrm{y}}=$ Grade of steel
$\mathrm{X}=0.77$ and 0.75 for steel grades of Fe 415 and Fe 500 respectively

- The point $1^{\prime}$ in fig- 2 corresponds to the axial loading condition with the mandatory minimum eccentricity $\mathrm{e}_{\text {min. }}$
- The point 3 in fig- 2 corresponds to the condition where neutral axis position is equal to the depth of the section i.e $x_{u}=D$ where $e=e_{d}$. For $e<e_{d}$, the entire column section is under compression and the neutral axis is located outside the section ( $\mathrm{X}_{\mathrm{u}}>\mathrm{D}$ ), with $0.002<\mathrm{e}_{\mathrm{cu}}<$ 0.0035 . For $e>e_{d}$, the neutral axis is located within the section ( $\mathrm{x}_{\mathrm{u}}<\mathrm{D}$ ), with $\mathrm{e}_{\mathrm{cu}}=0.0035$ at the highly compressed edge. Point 2 represents general case, with neutral axis outside the section ( $\mathrm{e}<\mathrm{e}_{\mathrm{d}}$ ).
- The point 4 in fig-2 corresponds to the balanced failure condition with both concrete and steel undergoing maximum yield thereby representing pure flexure condition.
- The point 5 in fig- 2 corresponds to the pure bending condition and at this stage the concrete suffers pure tensile failure.


Fig-2: Salient points on the interaction curve

## 3. METHODOLOGY

The procedure basically involves two stages design of interaction curve :

1. when neutral axis is inside the section
2. when neutral axis is outside the section.

## 3.1. $N$-A lies inside the section ( $K=X_{u} / D<1$ )

Step1:
Assume data like $\mathrm{f}_{\mathrm{y}}, \mathrm{f}_{\mathrm{ck}}$, Diameter of the bar
Step2:
Axial load carrying capacity of concrete (kN)
$\mathrm{P}_{\mathrm{uc}}=0.361 * \mathrm{f}_{\mathrm{ck}} *$ Area
Step3:
Axial load carrying capacity of steel $\mathrm{f}_{\mathrm{cc}}$

- $\mathrm{e}_{\mathrm{sc}}=0.0035\left[\mathrm{D}-\mathrm{d}^{\prime}\right] / \mathrm{D}$
- If $\mathrm{e}_{\mathrm{c}}>0.002$ then $\mathrm{f}_{\mathrm{cc}}=0.446 * \mathrm{f}_{\mathrm{ck}}$
- $\mathrm{e}_{\mathrm{c}}<0.002 \mathrm{f}_{\mathrm{cc}}=0.446{ }^{*} \mathrm{e}_{\mathrm{c}}{ }^{*} \mathrm{f}_{\mathrm{ck}}{ }^{*}\left[1-250 * \mathrm{e}_{\mathrm{c}}\right]$
- $P_{u s}=$ Stress in steel - stress in concrete
- Total Axial load, $P_{u}=P_{u c}+P_{u s}$
- Ultimate moment, $\mathrm{M}_{\mathrm{u}}=0.361 * \mathrm{f}_{\mathrm{ck}} * \mathrm{bd} *\left[\mathrm{C} . \mathrm{G}-\mathrm{d}^{\prime}\right]$


## 3.2. $N$-A lies outside the section ( $K=X_{U} / D<1$ )

- To find strain value:
- $\quad\left(0.0035-0.75^{*} \mathrm{e}_{\mathrm{cb}}\right) /(\mathrm{D}+0.1 \mathrm{D})=\mathrm{e}_{\mathrm{bb}} / 0.1 \mathrm{D}$
- $\mathrm{e}_{\mathrm{cu}}=0.0035-0.75 \mathrm{e}_{\mathrm{cb}}$
- $\quad \mathrm{Cc}{ }^{\prime}=\mathrm{Cc} /\left(\mathrm{f}_{\mathrm{ck}}{ }^{*} \mathrm{~B}^{*} \mathrm{D}\right)$ and $\mathrm{Yc}^{\prime}=\mathrm{Yc} / \mathrm{D}$
- $\quad \mathrm{Puc}_{\mathrm{uc}}=\mathrm{Cc}{ }^{\prime} \mathrm{f}_{\mathrm{ck}} * \mathrm{~B}^{*} \mathrm{D}$


## Stress calculation

- $\mathrm{e}_{\mathrm{cb}}=\mathrm{e}_{\mathrm{cu}}\left(\mathrm{D}-\mathrm{d}^{\prime}\right) / \mathrm{D}>0.002$
- If $\mathrm{e}_{\mathrm{c}}>0.002$ then $\mathrm{f}_{\mathrm{cc}}=0.446{ }^{*} \mathrm{f}_{\mathrm{ck}}$
- $\mathrm{e}_{\mathrm{c}}<0.002 \mathrm{f}_{\mathrm{cc}}=0.446^{*} \mathrm{e}_{\mathrm{c}}{ }^{*} \mathrm{f}_{\mathrm{ck}}{ }^{*}\left[1-250 * \mathrm{e}_{\mathrm{c}}\right]$
- $P_{\text {us }}=$ stress in steel - stress in concrete
- Total Axial load, $\mathrm{P}_{\mathrm{u}}=\mathrm{P}_{\mathrm{uc}}+\mathrm{P}_{\mathrm{us}}$
- Moment, $\mathrm{M}_{\mathrm{u}}=\left(\mathrm{C}_{\mathrm{c}}{ }^{*} \mathrm{f}_{\mathrm{ck}}{ }^{*} \mathrm{~B}^{*} \mathrm{D}\right){ }^{*}\left[\mathrm{CG}-\mathrm{Y}_{\mathrm{c}}{ }^{*} \mathrm{~d}\right]$

TABLE-1: Coefficients $C_{c}{ }^{\prime}$ and $Y_{c}{ }^{\prime}$ when the neutral axis lies outside the section

| $\mathbf{K}=\mathbf{X}_{\mathrm{u}} / \mathbf{D}$ | Coefficient $\mathbf{C}_{\mathrm{c}}{ }^{\prime}=\mathbf{C}_{\mathrm{c}} / \mathrm{f}_{\mathrm{ck}} \mathbf{B D}$ | Coefficient $\mathbf{Y}_{\mathrm{c}}{ }^{\prime}=\mathbf{Y}_{\mathrm{c}} / \mathbf{f}_{\mathrm{ck}} \mathbf{B D}$ |
| :---: | :---: | :---: |
| 1 | 0.361 | 0.416 |
| 1.05 | 0.374 | 0.432 |
| 1.1 | 0.384 | 0.443 |
| 1.2 | 0.399 | 0.458 |
| 1.3 | 0.409 | 0.468 |
| 1.4 | 0.417 | 0.475 |
| 1.5 | 0.422 | 0.480 |
| 2.0 | 0.435 | 0.491 |
| 2.5 | 0.44 | 0.495 |
| 3.0 | 0.442 | 0.497 |
| 4.0 | 0.444 | 0.499 |

## 4. RESULTS

Using Spread Sheet interaction curve were developed for Lshaped column and rectangle of same area of concrete and steel, in the developed excel sheet grades of cement, reinforcement spacing, size of sections etc can be modified. To develop interaction curve codes like SP -16 and IS: 4562000 is used ,the position of NA is placed at different points on the section including inside and outside. Values of $M_{u}$ and $\mathrm{P}_{\mathrm{u}}$ were calculated to plot the interaction curve.

## L SECTON :

COULMN SIZE : 600 X 600 mm
BREADTH : 200 mm

DIA OF BAR : 16 mm
NUMBER OF BARS : 16
GRADE OF CONCRETE : $30 \mathrm{~N} / \mathrm{mm}^{2}$
GRADE OF STEEL: $415 \mathrm{~N} / \mathrm{mm}^{2}$
NA VARIES ALONG WEB OF THE SECTION:


Fig-3: Dimensions of the L- sections considered for the analysis

Table-2: Values of $P_{u}$ and $M_{u}$ when NA is inside the section of the L section

| $\mathbf{N A}$ <br> $\mathbf{( m m})$ | Total axial load <br> carried by <br> column (kN) | Total moment <br> carried by column <br> $(\mathbf{k N}-\mathbf{m})$ |
| :---: | :---: | :---: |
| 0 | -1161.01 | -5.89215 |
| 33.6 | -943.11 | 71.0182 |
| 166.8 | -369.726 | 235.093 |
| 300 | 242.9077 | 321.508 |
| 433.2 | 1217.786 | 339.2851 |
| 566.4 | 2497.456 | 359.2177 |
| 600 | 2783.674 | 352.1417 |

Table-3: Values of $P_{u}$ and $M_{u}$ when NA is outside the section of the $L$ section

| NA <br> (mm) | Total axial load <br> carried by <br> column (kN) | Total moment <br> carried by <br> column (kN-m) |
| :---: | :---: | :---: |
| 630 | 2904.92 | 334.5598 |
| 660 | 3001.041 | 321.2904 |
| 720 | 3151.227 | 301.3147 |
| 780 | 3256.766 | 286.1581 |
| 840 | 3341.522 | 274.9822 |
| 900 | 3400.917 | 265.8135 |
| 1200 | 3551.617 | 242.88 |
| 1500 | 3611.407 | 233.5203 |
| 1800 | 3634.289 | 2292326 |
| 2400 | 3657.595 | 224.7906 |
| Infinity | 3687.65 | 0 |



Chart-1: Interaction curve for L-shape concrete column

NA VARIES ALONG FLANGE OF THE SECTION:


Fig -4: Dimensions of the L- sections considered for the analysis

Table-4: Values of $P_{u}$ and $M_{u}$ when NA is inside the section of the $L$ section

| $\mathbf{N A}$ <br> $\mathbf{( m m})$ | Total axial load <br> carried by column <br> $\mathbf{( k N})$ | Total moment <br> carried by <br> column $(\mathbf{k N}-\mathbf{m})$ |
| :---: | :---: | :---: |
| 0 | -1161.01 | 5.89 |
| 33.6 | -579.865 | 118.502 |
| 166.8 | 992.558 | 319.260 |
| 300 | 1886.366 | 299.630 |
| 433.2 | 2471.217 | 177.209 |
| 566.4 | 2955.848 | 27.045 |
| 600 | 3059.528 | -12.109 |

Table-5: Values of $P_{u}$ and $M_{u}$ when NA is outside the section of the $L$ section

| NA <br> (mm) | Total axial load <br> carried by <br> column (kN) | Total moment <br> carried by <br> column (kN-m) |
| :---: | :---: | :---: |
| 630 | 3153.22 | -41.474 |
| 660 | 3225.904 | -63.733 |
| 720 | 3337.381 | -97.173 |
| 780 | 3413.081 | -121.188 |
| 840 | 3473.081 | -139.462 |
| 900 | 3513.826 | -152.932 |
| 1200 | 3614.57 | -186.252 |
| 1500 | 3652.465 | -199.576 |
| 1800 | 3666.277 | -205.615 |
| 2400 | 3679.807 | -211.844 |
| Infinity | 3688.98 | 0 |



Chart-2: Interaction curve for L-shape concrete column

## RECTANGLE SECTION:

COULMN SIZE : 870 X 230 mm
DIA OF BAR : 16 mm
NUMBER OF BARS : 16
GRADE OF CONCRETE : $30 \mathrm{~N} / \mathrm{mm}^{2}$
GRADE OF STEEL : $415 \mathrm{~N} / \mathrm{mm}^{2}$


Fig -5: Dimensions of the rectangle sections considered for the analysis

Table-6: Values of $P_{u}$ and $M_{u}$ when NA is inside the section of the rectangle section

| NA <br> (mm) | Total axial load <br> carried by <br> column (kN) | Total moment <br> carried by <br> column (kN-m) |
| :---: | :---: | :---: |
| 0 | -1161.01 | 0 |
| 50 | -891.33 | 107.46 |
| 160 | -332.46 | 210.22 |
| 270 | 226.84 | 421.02 |
| 380 | 786.584 | 484.62 |
| 490 | 1345.13 | 490.89 |

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| 600 | 1861.57 | 453.97 |
| :---: | :---: | :---: |
| 710 | 2287.57 | 403.19 |
| 820 | 2789.91 | 283.92 |
| 870 | 2963.64 | 239.14 |

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Table-7: Values of $P_{u}$ and $M_{u}$ when NA is outside the section of the rectangle section

| NA (mm) | Total axial load <br> carried by <br> column (kN) | Total moment <br> carried by <br> column (kN-m) |
| :---: | :---: | :---: |
| 913.5 | 3066.71 | 205.66 |
| 957 | 3147.31 | 180.40 |
| 1044 | 3272.05 | 142.48 |
| 1131 | 3357.9 | 114.73 |
| 1218 | 3426.42 | 93.97 |
| 1305 | 3471.46 | $78 . .26$ |
| 1740 | 3591.51 | 38.24 |
| 2175 | 3635.75 | 23.49 |
| 2610 | 3653.17 | 16.27 |
| 3480 | 3670.81 | 8.81 |
| Infinity | 3688.98 | 0 |



Chart-3: Interaction curve of Rectangular section.
For the rectangle section of ( $870 \times 230$ ) mm we get the $B / D=0.264$, Similarly, $B / D$ ratio of rectangle is varied but the area of steel and concrete is kept same. The interaction diagram of L-section is compared with rectangular of different $\mathrm{B} / \mathrm{D}$ ratio column and it is shown below.


Chart-4: Interaction curve of L section compared with rectangle concrete column of $B / D=0.264$

Chart-4 to Chart-9 represent the interaction curve of L section where HCE is consider along web section compared with the rectangle section of different $B / D$ ratio.

Chart-10 to Chart-15 represent the interaction curve of L section where HCE is consider along flange section compared with the rectangle section of different B/D ratio.


Chart-5: Interaction curve of $L$ section compared with rectangle concrete column of $B / D=0.449$


Chart-6: Interaction curve of L section compared with rectangle concrete column of $B / D=0.612$


Chart-7: Interaction curve of L section compared with rectangle concrete column of $B / D=0.799$


Chart-8: Interaction curve of L section compared with rectangle concrete column of $B / D=1.01$


Chart-9: Interaction curve of L section compared with rectangle concrete column of $B / D=1.24$


Chart-10: Interaction curve of L section compared with rectangle concrete column of $B / D=0.264$


Chart-11: Interaction curve of $L$ section compared with rectangle concrete column of $B / D=0.448$


Chart-12: Interaction curve of L section compared with rectangle concrete column of $B / D=0.612$


Chart-13: Interaction curve of $L$ section compared with rectangle concrete column of $B / D=0.799$


Chart-14: Interaction curve of $L$ section compared with rectangle concrete column of $B / D=1.01$


Chart-15: Interaction curve of $L$ section compared with rectangle concrete column of $\mathrm{B} / \mathrm{D}=1.24$

## 5. CONCLUSIONS

The paper involves comparing the behavior of L-shaped column when its area of steel and area of concrete is kept same as that of the rectangle section. The results obtained in the work leads to the following conclusions.

- The ultimate load carrying capacity of L section where HCE consider at web when compared with rectangle shows $0.036 \%$ variation which can be concluded that load carrying capacity will be same for both sections since area of steel and concrete kept same.
- As we change the size of rectangular section the ultimate moment carrying capacity varies, here comparison is made when HCE is consider at web and variation 27.456, 8.77, 2.06 \% decrease as B/D ratio of rectangular section $0.264,0.449,0.612$ varied respectively and 11.09, 18.77, $24.529 \%$ increase as $B / D$ ratio of rectangular section 0.799 , 1.01, 1.24 varied respectively.
- similarly, ultimate load carrying capacity of L section where HCE consider at flange is compared with rectangle shows $0.036 \%$ variation.
- Similarly, the size of rectangular section varied the ultimate moment carrying capacity when HCE is consider at flange and capacity $35.52,18.924,9.24$ \% decrease as B/D ratio of rectangular section $0.264,0.449,0.612$ varied respectively and we observe that there will be $0.02 \%$ variation when compared with $\mathrm{B} / \mathrm{D}$ ratio of 0.799 of rectangular section and there is $8.62,15.024 \%$ increase as B/D ratio of rectangular sectiona1.01, 1.24 varied respectively.


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