

# **STRENGTH PROVISION OF RC BUILDINGS BY USE OF MODIFIED**

# **SHEAR WALL**

Chandan Kumar<sup>1</sup>, Gaurav Tanwar<sup>2</sup>

<sup>1</sup>M.Tech research scholar, Department of Civil Engineering, BRCM CET, Bahal <sup>2</sup>Assistant professor, Department of Civil Engineering, BRCM CET, Bahal \*\*\*

**Abstract** – This study presents the strength imparting technique to the shear walls when subjected to reverse cyclic loading. If the proposed technique is used, there is no need for vacating the building during renovation, so there is no disturbance for occupants or users during strengthening and rehabilitation. Shear walls are installed in parallel direction to the exterior side of buildings in this proposed. The findings of this technique are such as there is quite improve in the capacity and sway stiffness of reinforced concrete structures. Also shear walls which were attached later, behave as a monolithic member of structure. This technique can be better utilized in India where we have a huge population and during renovation work of a building we have to vacate the building which ultimately disturbs the living life of humans. By this technique we not only strengthened the existing building quickly but this method also found to be more economical as compared to the other methods of Strengthening of vulnerable buildings which was not constructed according to modern code provisions. As day by day seismic zones are changing the buildings which are earlier not prone to Earthquake, now came in severe zones, so for them this method of strengthening may be done very easily. We can provide sufficient stiffness to the building to resist the lateral loads significantly by constructing exterior shear wall of adequate strength as per Code provisions.

This present study consists of the structural model having (G+8) storey, symmetrical along both the longitudinal and lateral directions simultaneously. The models are subjected to the external lateral loads in the form of seismic loads. The building is subjected to different load combinations as per the code recommends and base shear, displacement, drift values, time period, forces in columns and beams were obtained at different storey level. In addition to this, the same model is provided with the use of external shear walls along the same direction of loading in plan and provides a connection to external shear wall system with the beams and columns of existing building using links of (25 mm dia. HYSD bars of Fe-415). The analysis is subjected to various combinations of loads as per the IS codes. It is observed that lateral displacement of the structure, value of storey drift gets reduced to a reasonable extent which is within the permissible limit. Also this time those members which was found to be weak in carrying the lateral forces due to less stiffness earlier, are now strong enough in carrying lateral load.

# **1. INTRODUCTION**

Earthquake is one of the major disasters natural hazards that cause huge loss of life, livelihood and natural vegetation. According to various studies & surveys, an average about 10000 people die each year due to earthquake, while economic losses are in billions of dollars and Gross National Product of a country is largely affected.

Earthquake is caused by instant release of energy in earth crust which shakes earth's crust. Earthquake is measured by richter's scale and is plotted on seismograph.

# **1.1 SHEAR WALL**

Shear Wall is the structural component which consists of shear panels / braced panels that resist the effect of transverse loads acting on structures. Shear wall are designed to bear wind and seismic load.

# **1.2 TYPE OF COUPLED SHEAR WALLS**

Shear walls which have opening at various positions are known as coupled shear walls.

- **One Row:** -These coupled shear walls which have opening in single vertical row are called one row shear wall.
- **Two Row:** Shear wall having two row of vertical opening parallel to each other are known as two row shear wall.
- Staggered Row: Shear walls having opening not in same vertical line but in alternate rows are called staggered rows.



# 2. RESEARCH OBJECTIVES

This thesis aims to know the effect of external shear wall connection to the existing building for strengthening purpose to resist the lateral load acting on it. The main research objectives of this present study are given as:

- 1. Formation of models (G+8) having Rigid Diaphragm using ETABS platform.
- 2. The model is subjected to earthquake load in both x and y direction. Considering the building symmetrical in plan and is located in zone IV on medium soil strata site.
- 3. Analyse of lateral displacement in both direction, storey shear forces, modal information, Column forces, beam forces etc.
- 4. Again another model as model 2, of same dimension and properties as of model 1, is created but this time external shear wall are connected to the building model with the help of steel bars as links and then the result of same parameters, as for model -1 is obtained.
- 5. Again another model as model 3, is created same as that of model 2, but this time opening are provided in the external shear wall and the model is analysed, then for same parameters results are obtained.

## **3.1 MATERIAL PROPERTIES**

The material properties used in creating the model were as follows:-

- 1. Concrete Grade M 20 (in case of Beams) and M 25 (In case of Columns)
- 2. Grade of Steel Used HYSD Bars (Fe-415)
- 3. Poisson Ratio of Steel 0.3
- 4. Poisson Ratio of Concrete 0.2
- 5. Young's Modulus of concrete 25000000KN/m<sup>2</sup> (M25) 22360000KN/m<sup>2</sup> (M20)
- 6. Young's Modulus of reinforcement  $2.1 X 10 10 \ KN/m^2$
- 7. Damping Factor 0.05

## **3.2 GEOMETRIC PROPERTIES**

The geometrical properties measured and used to create model were as follows:

- 1. The slab thickness 125 mm
- 2. Beam cross sections on all floors 0.3mX0.50m
- 3. Column cross section on all floors 0.3mX0.75m
- 4. Storey Height 3.5m on the lower most story 3.0m on all the above stories
- 5. Spans 5.0m x 5.0m
- 6. Link1 of steel bars = 25mm
- 7. Wall thickness = 200mm

# **3.3 LOADING**

- 1. Self Weight of Structure is taken on the basis of their cross-section.
- 2. Imposed Load over the frame is taken as 4 KN/m<sup>2</sup> (On the Basis of Commercial Structures)
- 3. Brick wall load= 6.875 KN/m
- 4. Parapet wall load on top storey is = 3 KN/m

#### **3.4 DESCRIPTION OF MODELS:**

	Model – 1	Model – 2	Model – 3
No. of Storey	G + 8	G + 8	G + 8
Seismic Zone	IV	IV	IV
Soil Type	Medium	Medium	Medium
Storey Height	Ground Storey = 3.5m	Ground Storey = 3.5m	Ground Storey = 3.5m
	Above Storey = 3.0m	Above Storey = 3.0m	Above Storey = 3.0m
Size of Beams	0.3 m x 0.5 m	0.3 m x 0.5 m	0.3 m x 0.5 m
Size of Columns	0.3m x 0.75m	0.3m x 0.75m	0.3m x 0.75m



International Research Journal of Engineering and Technology (IRJET)

Volume: 07 Issue: 09 | Sep 2020

www.irjet.net

e-ISSN: 2395-0056 p-ISSN: 2395-0072

Roof and Floor Thickness	125 mm	125 mm	125 mm
Thickness of Shear Wall	No shear Wall is	External Shear Wall of	External Shear Wall of 200mm
	provided	200mm Thickness	Thickness with openings
Material Used	M20, M25, Fe-415	M20, M25, Fe-415	M20, M25, Fe-415

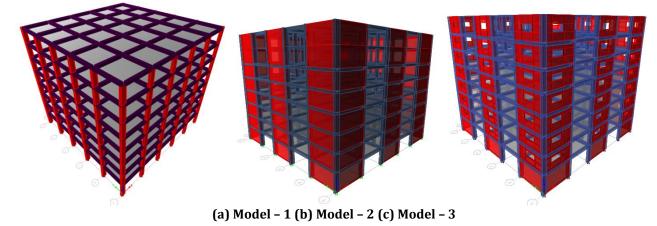


Fig. 1: 3-D View of Various Models Considered

# 4. RESULTS AND ANALYSIS

## 4.1 FUNDAMENTAL TIME PERIOD OF VIBRATION UNDER VARIOUS MODES

Table 2: Time Period of Vibration for Model 1											
Information of Model 1											
Mode	Period	UX	UY	UZ	Sum UX	Sum UY					
	sec										
1	2.234	0	0.8712	0	0	0.8599					
2	1.732	0.00613	0.0011	0	0.00623	0.8598					
3	1.621	0.8125	0.01	0	0.8234	0.8598					
4	0.699	0	0.0911	0	0.8012	0.9619					
5	0.501	0.0012	1.61E-06	0	0.834	0.9619					
6	0.5	0.1131	0	0	0.899	0.9619					
7	0.409	0	0.031	0	0.899	0.9651					
8	0.274	0	0.0132	0	0.899	0.9818					
9	0.261	5.99E-06	5.123E-06	0	0.9201	0.9312					
10	0.249	0.0411	0	0	0.9610	0.9312					

## **Table 3:** Time Period of Vibration for Model 2

	Information of Model 2										
Mode	Period	UX	UY	UZ	Sum UX	Sum UY					
	sec										
1	0.635	0	0.7129	0	0	0.7129					
2	0.615	0.7152	0	0	0.7152	0.7129					
3	0.379	0	0	0	0.7152	0.7129					
4	0.165	0	0.195	0	0.7152	0.9079					
5	0.16	0.1907	0	0	0.9059	0.9079					
6	0.096	0	1.93E-06	0	0.9059	0.9079					
7	0.094	0	0.0518	0	0.9059	0.9598					
8	0.091	0.0501	0	0	0.956	0.9598					
9	0.075	0	0.0177	0	0.956	0.9775					
10	0.07	0.0177	0	0	0.9736	0.9775					



Table 4: Time Period of Vibration for Model 3										
Information of Model 3										
Mode	Mode Period UX UY UZ Sum UX									
	Sec									
1	0.662	7.83E-06	0.7117	0	7.83E-06	0.7117				
2	0.637	0.7152	7.86E-06	0	0.7152	0.7117				
3	0.397	0	0	0	0.7152	0.7117				
4	0.176	0	0.1852	0	0.7152	0.8969				
5	0.17	0.1815	0	0	0.8967	0.8969				
6	0.103	0	0	0	0.8967	0.8969				
7	0.101	0	0.0513	0	0.8967	0.9481				
8	0.096	0.0506	0	0	0.9473	0.9481				

From above tables we can confirm that as less stiffness structures or rather flexibility have more time period for different modes, as this can be seen from table of model-1.

As soon as the stiffness is provided to the structure with the help of external shear wall, now time period of different modes comes out to be lesser than that of model – 1. We can see from table of modal information that for 1st mode time period of model- 1 is 2.169 seconds and for model – 2 for the same mode time period is 0.635 seconds. But again in model – 3 time period of mode 1 is increased a little bit to the value 0.662 seconds, because by providing opening in the shear wall stiffness of the structure as a whole has been reduced to some extent.

# 4.2 COLUMN FORCES RESULTS OF C36 LOCATED AT STOREY 1 DUE TO EQX AND EQY LOAD

Building framed structure without external shear wall										
Story	Column	Load Case/Combo	Р	V2	V3	Т	M2	М3		
			kN	kN	kN	kN-m	kN-m	kN-m		
Story1	C36	EQ X	517.58	48.4271	0.2306	0.0376	0.1701	167.802		
Story1	C36	EQ X	517.58	48.4271	0.2306	0.0376	-0.1798	93.3849		
Story1	C36	EQ X	517.58	48.4271	0.2306	0.0376	-0.5045	16.8043		
Story1	C36	EQ Y	489.23	0.1034	33.6676	-0.0109	81.4517	-0.8151		
Story1	C36	EQ Y	489.23	0.1034	33.6676	-0.0109	26.2073	-0.9603		
Story1	C36	EQ Y	489.23	0.1034	33.6676	-0.0109	-32.751	-1.0832		

**Table 5:** Value of Column Forces at Storey 1 of Model - 1

**Table 6:** Value of Column Forces at Storey 1 of Model - 2

	Building framed structure with shear wall without opening											
Story	Column	Load Case/Combo	Р	V2	V3	Т	M2	M3				
			kN	kN	kN	kN-m	kN-m	kN-m				
Story1	C36	EQ X	245.23	13.2779	-0.3384	0.3513	-0.3255	43.2538				
Story1	C36	EQ X	245.23	13.2779	-0.3384	0.3513	0.1995	22.626				
Story1	C36	EQ X	245.23	13.2779	-0.3384	0.3513	0.6816	1.1818				
Story1	C36	EQ Y	217.28	-1.7205	1.8167	-0.3653	7.347	-1.441				
Story1	C36	EQ Y	217.28	-1.7205	1.8167	-0.3653	3.8851	1.1557				
Story1	C36	EQ Y	217.28	-1.7205	1.8167	-0.3653	-0.4213	3.7108				

Buildin Story

> Story1 Story1 Story1 Story1 Story1

> Story1

C36

	Tuble 7. Value of column Forces at storey 1 of Model 5											
<b>ig</b> 1	g framed structure with external shear wall with the openings provided											
	Column	Load Case/Combo	Р	V2	V3	Т	M2	M3				
			kN	kN	kN	kN-m	kN-m	kN-m				
	C36	EQ 1	248.56	9.8958	1.4353	0.4096	1.8814	37.7751				
-	C36	EQ 1	248.56	9.8958	1.4353	0.4096	-0.3987	22.321				
	C36	EQ 1	248.56	9.8958	1.4353	0.4096	-2.5964	6.088				
-	C36	EQ 2	221.69	7.5404	1.1978	-0.381	6.2564	8.9946				
	C36	EQ 2	221.69	7.5404	1.1978	-0.381	3.8328	-2.4308				

7.5404

1.1978

-0.381

0.603

-13.772

Form above table for three models in combined form, we clearly see that in model-1 all the values for forces comes out to be more than that of when compared with model-2 and model-3, because in model-1 case, for EQX and EQY load acting at the storey level 1, most of the load is taken by framed structure as there is no special lateral load resisting element in the building (like shear wall) but in model-2 and model-3 Now most of the lateral load due to EQX and EQY is taken by the external shear wall which is created, so forces acting on the column members comes out to be less in value, Here we see a clear decrease in forces for the strengthened models withshear wall (Model-2 & Model-3). This clearly shows that the shear walls are playing its part in taking the lateral forces due to earthquake force.

221.69

# 5) BEAM FORCES RESULT OF B51 AT STOREY 8 LEVEL DUE TO EQX LOAD

EO 2

			Μ	odel 1	Model 2		Model 3	
Storey	Beam	Load Case/Combo	Shear force V2	MomentM3	Shear force V2	MomentM3	Shear force V2	MomentM3
			kN	kN-m	kN	kN-m	kN	kN-m
Story8	B51	EQX	11.5177	21.962	8.298	12.69	8.1173	11.695
Story8	B51	EQX	11.5177	16.922	8.298	11.69	8.1173	8.1432
Story8	B51	EQX	11.5177	11.883	7.956	9.023	7.0812	8.0079
Story8	B51	EQX	10.1967	11.692	7.956	6.59	7.0812	5.0575
Story8	B51	EQX	10.1967	7.4436	7.956	4.235	7.0812	2.1069
Story8	B51	EQX	10.1967	3.1948	7.956	-1.296	7.0812	-0.844
Story8	B51	EQX	10.1967	-1.054	7.125	-1.223	6.9916	-0.992
Story8	B51	EQX	10.1388	-1.271	7.125	-4.035	6.9916	-3.905
Story8	B51	EQX	10.1388	-5.496	7.125	-6.912	6.9916	-6.818
Story8	B51	EQX	10.1388	-9.722	7.125	-9.965	6.9916	-9.731
Story8	B51	EQX	10.1388	-13.95	7.6511	-10.235	7.6511	-9.872
Story8	B51	EQX	10.8321	-14.16	7.6511	-13.564	7.6511	-13.22

Table 8: Beam Forces Result of B51 at Storey 8 Level

From the above table results we can say that by providing external shear wall in strengthened models as (model - 2, and model - 3). we have also reduced the load that is acting on the beams because shear wall created are taking most the load thus loads value has been decreased to a reasonable amount which shows that even weak beams do not fails due the above load and remains at stronger side.

#### 6.2 Conclusion

From this study and the results obtained it is being concluded that the buildings which was constructed before the introduction of modern codes but their importance value is more (such as schools, hospitals, fire stations and power stations etc. Such buildings cannot sustain the lateral load (mainly earthquake load) effectively as these were not designed for these loads or due to various types of faulty construction work.

But now as seismic zones are changing day by day and now these buildings exist in severe to very severe zones we cannot vacate these building for a longer period during renovation work, which causes disturbance to the living life of population.

- From this study and its outcomes clearly indicates that we can strengthened these building by inspecting the degree of their vulnerability, by the use of external shear walls along the parallel sides of the building and connection can be made effectively between the exterior shear wall and existing building using dowel bars of sufficient diameter (steel bars) to act as a monolithic structure during lateral forces acting on it.
- From that stiffness of the structure can be increased as a whole and most of the lateral loads is taken by the shear wall, with the help of which the structures can be damaged to a lesser extent.
- This method is also of a great importance that instead of doing elemental strengthening of building
- Thus various parameters like displacement, storey shear, time period, forces in column and beams have been reduced to a greater percentage which makes the building on stronger side then earlier condition.

# REFERENCES

- [1] Hasan Kaplan, Salih Yilmaz, Nihat Cetinkaya And Ergin Atimtay, Seismic Strengthening Of RC Structures With Exterior Shear Walls, Indian Academy of Sciences sadhana Vol. 36, Part 1, February 2011, pp. 17–34.
- [2] Wylli Jr., Guidelines for Epoxy Grouted Dowels in Seismic Strengthening Projects, Ninth world conference on Earthquake Engineering, August 2-9,1988, Tokyo, JAPAN (Vol. III).
- [3] K. galal And H. El-sokkary, Recent Advancements in Retrofit of RC Shear Walls, The 14<sup>th</sup> World Conference on Earthquake Engineering October 12-17, 2008, Beijing, China
- [4] M. Y. Kaltakci, M.Ozturk, And M. H. Arslan., An Experimental Investigation for External RC Shear Wall Applications, Natural hazards and earth system sciences, 16 Sep2010
- [5] Guideline for Seismic Upgrading Of Building Structures, National Research Council of Canada, December 1995. ISBN 0-660-16262-8, NRCC 38857
- [6] Venkata Sairam Kumar.N, Surendra Babu.R, Usha Kranti.J.International Journal Of Innovative Research In Science, Engineering And Technology,Vol. 3, Issue 2, February 2014 ,(An ISO 3297: 2007 Certified Organization).
- [7] Dr. Durgesh C. Rai, Seismic Evaluation and Strengthening Of Existing Buildings, Indian Institute of Technology Kanpur.
- [8] A. Okakpu, G. Ozay, decision selection technic for building strengthening methods, Asian Journal Of Civil Engineering (Bhrc) VOL. 16, NO. 2 (2015), PAGES 203-218
- [9] Plain and Reinforced Concrete-Code Practice IS:456 : 2000
- [10] Criteria for Earthquake Resistant Design Of Structure IS 1893 : 2002
- [11] Ductile Detailing Of ReinforcedConcrete Structures Subjected ToSeismic Forces -Code Of Practice IS13920: 1993
- [12] ACI Committee 318 2005 Building code requirements for structural concrete and commentary (ACI 318M-05). American Concrete Institute
- [13] Albanesi T, Biondi S, Candigliota E and Nuti C 2006 Experimental analysis on a regular full scale infilled frame. Proceedings of the First European Conference on Earthquake Engineering and Seismology, Geneva, Paper No. 1608
- [14] Altın S, Ersoy U and Tankut T 1992 Hysteretic response of reinforce concrete infilled frames. ASCE J. Struct. Eng., 118(8): 2133–2150
- [15] Baran M 2005 Precast concrete panel infill walls for seismic strengthening of reinforced concrete framed structures. PhD thesis, Middle East Technical University, Ankara
- [16] Bass R A, Carrasquilloi R L and Jirsa J O 1989 Shear transfer across new and existing concrete interfaces. ACIStruct.J.,86(4): 383–393
- [17] Bush T D, Wyllie L A and Jirsa J O 1991 Observations on two seismic strengthening schemes for concrete frames. Earth. Spectra, 7(4): 511–527
- [18] Canbay E, Ersoy U and Ozcebe G 2003 Contribution of reinforced concrete infills to seismic behaviour of structural systems. ACI Struct. J., 100(5): 637–643
- [19] CSI, SAP2000 V-8 2002 Integrated finite element analysis and design of structures basic analysis reference manual. Berkeley, California (USA): Computers and Structures Inc.
- [20] Federal Emergency Management Agency, FEMA-356 2000 Prestandard and commentary for seismic reha- bilitation of buildings. Washington (DC)
- [21] Frosch R J, Wanzhi L, Jirsa J O and Kreger M E 1996 Retrofit of non-ductile moment-resisting frames using precast infill wall panels. Earth. Spectra, 12(4): 741–760



- [22] Gilmore A T, Bertero V V and Youssef N F G 1996 Seismic rehabilitation of infilled non-ductile frame buildings using posttensioned steel braces. Earth. Spectra, 12(4): 863–882
- [23] Harris H G and Sabnis G M 1999 Structural modeling and experimental techniques. 2nd ed, Florida: CRC Press Inc
- [24] Higashi Y, Endo T and Shimizu Y 1982 Effects on behaviours of reinforced concrete frames by adding shear walls. Proceedings of the Third Seminar on Repair and Retrofit of Structures, Michigan, pp. 265–290
- [25] Hognestad E A (1951) Study of combined bending and axial load in RC Members Engineering Experi- mental Station Bulletin Series No. 399, University of Illinois
- [26] Inel M and Ozmen H B 2006 Effects of plastic hinge properties in nonlinear analysis of reinforced concrete buildings. Eng. Struct., 28(11): 1494–1502
- [27] Jirsa J and Kreger M 1989 Recent research on repair and strengthening of reinforced concrete structures. Proceedings of the ASCE Structures Congress, California, 1: 679–688
- [28] Kaplan H, Yılmaz S, Cetinkaya N, Nohutcu H and Atımtay E Gönen H (2009) A new method for strengthening of precast industrial structures. J. of the Faculty of Eng. and Archit. of Gazi Univ., 24(4): 659–665, (in Turkish)
- [29] Kaltakci M Y, Arslan M H, Yilmaz U S and Arslan H D 2008 A new approach on the strengthening of primary school buildings in Turkey: An application of external shear wall. Build. and Environ., 43(6): 983–990.
- [30] Mander J B 1984 Seismic design of bridge piers. Research report 84-2, Christchurch (New Zealand), Department of Civil Engineering, University of Canterbury
- [31] Mander J B, Priestley M J N and Park R 1988 Theoretical stress–strain model for confined concrete. ASCEJ. Struct. Eng., 114(8): 1804–1826
- [32] Masri A and Goel S 1996 Seismic design and testing of an RC slab-column frame strengthened with steel bracing. Earth. Spectra, 12(4): 645–666