

# ANALYSIS AND DESIGN OF COMPOSITE STEEL BRIDGE GIRDER

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**Abstract** – Steel- Concrete composite structures have been used in bridge engineering from decades. This is due to rational utilization of the strength properties of two materials. The most commonly found in practice are composite girder bridges, particularly in highway bridges of small and medium spans in larger spans steel truss girders are applied. Bridge Composite structures are also employed in cable-stayed bridge decks the main girder spans. The aim of the article is to present the construction process and strength analysis problems concerning of this type of structures. Attention is paid to the design and calculation of the shear connectors characteristic for the discussed objects.

**Key Words:** Cable Stayed bridge, decks, Strength, Analysis.

## 1. INTRODUCTION

A composite material is basically a combination of two or more materials, each of which retains its own distinctive properties. Multiphase metals are composite materials on a micro scale, but generally the term composite is applied to materials that are created by mechanically bonding two or more different materials together. Composite is applied to materials that are created by mechanically bonding two or more different materials together. The resulting material has characteristics that are not characteristic component of isolation. Composites offer many benefits the key among them are corrosion resistance, design flexibility, durability, light weight and strength.

**1.1 COMPOSITE STRUCTURES :** Composite means that the steel structures of a bridge is fixed to the concrete structure of the deck so that the steel and concrete act together, so reducing deflections and increasing strength. This is done using 'shear connectors' is fixed to the steel beams and then embedded in the concrete. Shear connectors can be welded on, perhaps using a 'stud welder', or better still on export work, by finding nuts and bolts.

## 1.2 OBJECTIVES OF THE PROJECT:

To achieve the objectives of the current design, steel concrete composite bridges (SCCB) can be a good alternative due to the recyclability of steel parts of the structure, have been used extensively since the 20<sup>th</sup> century when composite structure theories were developed more generally.

## 2. ANALYSIS OF THE STRUCTURE

The composite bridges are of either multi-girder or ladder form. Determining the principal effects of the various loading combinations can often be achieved with a 2-dimensional analytical model but not for a more comprehensive analysis a 3-dimensional model analysis model is needed. This article reviews the appropriate analysis and modeling techniques. There are three modeling options for a typical multi-girder steel composite bridge. There are Line beam, Grillage, Full Finite element model.

## ANALYSIS OF LOADS :

There are two types of loads which are considered in the analysis. Dead load, Live Load. Dead Load : It is constant load in a structure that is due to the weight of the members, the supported structure and permanent attachments. Live Load : Live loads are calculated by using the codes for design of various type of loads.

## 3. DESIGN OF COMPOSITE STRUCTURE :

### 3.1 Data :

Effective Span = 30m

Spacing of girders = 3m

Web Section = 2100 x 12mm

Top Flange = 450 X 25mm

Bottom Flange = 600 x 40mm

Slab = 4000x 200mm deep

Fillet on top of top flange = 750mm

Self weight of girder= 9.6 KN

Total DL + SDL per girder = 1109 KN

Wind load on girder = 4.63KN(as per IS 10262)

Wind on Vehicle = 5.15 KN

**Table 3.1: Section 1 Non-composite**

**Component Area  $Y_i$   $A \cdot Y_i$   $m^3$   $Y_i - Y_{sb}$   $I_g$   $AY_i^2$   $I_{xx} = I_g + A$**

**$(Y_i - Y_{sb})^2$**

Top Flange 11250 2152.5 24215625 1289.6 585938 187.10 1.87x

$\times 10^8$   $10^{10}$

Web 25200 1090 27468000 227.1 9.26 105.10 1.06x

$\times 10^8$   $10^{10}$

Bottom 24000 20 480000 -842.9 320000 171.10 1.71x

flange  $\times 10^8$   $10^{10}$

Total 60450 862.9 52163625 9.26x 463.10 4.63 x

$10^9 \times 10^8$   $10^{10}$

$Z_1$  on top of steel girder =  $4.63 \times 10^{10} / (1289.6 + 125) = 35578131 \text{ m}^3$

$Z_b$  at bottom flange of girder =  $4.63 \times 10^{10} / 863 = 53684477 \text{ m}^3$

**Table 3.2 :**

**Section 2 : Composite Short term**

With  $m=8$

**Component Area  $Y_i$   $A \cdot Y_i$   $m^3$   $Y_i - Y_{sb}$   $I_g$   $AY_i^2$   $I_{xx} = I_g + A$**

**$(Y_i - Y_{sb})^2$**

Top Flange 11250 2152.5 24215625 620.9 585938 4.34 4.34x

$\times 10^9$   $10^9$

Web 25200 1090 27468000 -441.6 9.26 105.10 1.06x

$\times 10^9 \times 10^9$   $10^{10}$

Bottom 24000 20 480000 -1511.6 320000 5.48 5.48x

flange  $\times 10^{10}$   $10^{10}$

Top slab 50000 2340 1.17E+8 808.4 1.67x 3.27x 3.28

=  $2000 \times 10^8$   $10^{10} \times 10^{10}$

200/8

Total 60450 862.9 52163625 9.43x 9.68 1.06 x

$10^9 \times 10^{10}$   $10^{11}$

$$Z_b = 1.06 \times 10^{11} / (620.9 + 12.5) = 1.68 \times 10^8$$

$$Z_t = 1.06 \times 10^{11} / 1531.6 = 0.70 \times 10^8$$

$$Z_{tc} \text{ in slab} = 1.06 \times 10^{11} / (808.4 + 100) = 1.17 \times 10^8$$

**Table 3.3 ;**

**Condition 3 for long term**

With increased modular ratio of 16

**Component Area  $Y_i$   $A \cdot Y_i$   $m^3$   $Y_i - Y_{sb}$   $I_g$   $AY_i^2$   $I_{xx} = I_g + A$**

**$(Y_i - Y_{sb})^2$**

Top Flange 11250 2152.5 24215625 1289.6 585938 8.27 82.70x

$\times 10^9$   $10^8$

Web 25200 1090 27468000 227.1 9.26 1.03 103x

$\times 10^9 \times 10^{10}$   $10^8$

Bottom 24000 20 480000 -1511.6 320000 3.9 390x

flange  $\times 10^{10}$   $10^8$

Top slab 50000 2340 1.17E+8 808.4 0.88x 2.74x 274

=  $2000 \times 10^8$   $10^{10} \times 10^{10}$

200/8

Total 60450 862.9 52163625 - 9.35x 7.56 850x

$10^9 \times 10^{10}$   $10^8$

$$Z_b = 0.85 \times 10^{11} / (857.4 + 12.5) = 97.70 \times 10^6$$

$$Z_t = 0.85 \times 10^{11} / 1295.1 = 65.63 \times 10^6$$

$$Z_{tc} \text{ in slab} = 0.85 \times 10^{11} / (1044.9 + 100) = 77.24 \times 10^6$$

Hence the design is safe when compared with non -Composite section than Composite Section.

**4. CONCLUSIONS**

Composite Steel- Concrete decks are particularly well designed to work in mid-span regions. The top concrete slab withstands the compressive forces While the bottom steel structure copes with the tensile forces generated by the positive bending moments. However these composite decks are less efficient for the negative bending moments over the intermediate support cross sections. On one hand, the slab of concrete tends to crack under the tensile forces, and significant quantities of reinforcing are needed to control this effect. On the other hand the steel structure below needs stiffeners to ensure its high resistance to compression,

without local or global instability. Decks with double composite action are a recent development in this structural solution in which the second slab of concrete is added to bottom flange of steel structure.

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